

DESIGN AND IMPLEMENTATION OF SHORT-RANGE WIRELESS TRANSMISSION WITH LOW PASS FILTER FOR WLAN APPLICATION

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ABSTRACT

A low pass microwave filter and a short line wireless transmission were created. The filters to use the step extracts the features, with the characteristic linear impedance of alternative parts either being too high or too low. This filter is now encouraged by using HFSS apps and reliance on full-wave analytical techniques in a three-dimensional work site to modify each high or low resistance value such as width and length desirable properties can be rich. Once evolved with micro strip technology, it becomes practical. This filtration is much less complex than others. The outcomes of creating an effective and modelling were all fairly consistent.

Keywords: Low pass, microwave filter, wireless, impedance, length, micro strip

1. INTRODUCTION

Microwaves are a type of electromagnetic radiation with wave lengths from about one meter to one millimetre, corresponding to frequencies ranging from 300 MHz to 300 GHz. Different sources define microwaves as different frequency ranges; above that the broad definition includes all these UHF and EHF (mm wave) bands. [3]. Signals are electromagnetic waves with wavelengths ranging from 1 to 10mm [4]. They are located in the electromagnetic between visible energy and radio waves. Microwaves travel in a straight line [5]; unlike shorter wavelength radio waves, microwaves do not refract around cliffs, obey an earth's crust as vibrational modes [6], or reflect from the ionosphere, curtailing microwave radio data transmission to about 40 miles (64 km) [7]. Those who have been swallowed up by carbon in the air will limit useful conversation ranges to around a kilometre in [8].

2. METHODOLOGY

The suggested band stop filter's basic structure relies just on sections. the first section transmission line stub network shown. The filtration characteristics of this filtration system are entirely essential to the design of character trait characteristic impedance Z_i for open-circuited stubs, Z_i , $i+1$ for unit elements, and two aborting characteristic impedance Z_A and Z_B [8,9].

The synthesis of the above shown ladder network

$$|S_{21}(f)|^2 = 1/1 + E^2 A_n^2(f) \quad (1)$$

Where is the band pass filter ripple continuous and A_n is indeed the filtration function defined by the function shown below.

$$A_n(f) = B_n(t/t_c) B_{n-1}(t\sqrt{i-t}/t\sqrt{i-t}) - C_n(t/t_c) C_{n-1}(t\sqrt{i-t}/t\sqrt{i-t}) \quad (2)$$

Where t is the Richards' transform variable which is given by

$$t = j \tan\left(\frac{\pi}{2} * f/f_0\right) \quad (3)$$

$$T_c = j \tan(\pi/4(2 - FBW)) \quad (4)$$

$$FBW = f_2 f_1 / f_0 * 100\% \quad (5)$$

Where f_0 is the band-stop filter's mid-band frequency, FBW is the partial bandwidth, and the Chebyshev features of the first and 2nd kinds of order n

$$B_n(x) = \cos(n \cos^{-1} x) \quad (6)$$

$$C_n(x) = \sin(n \cos^{-1} x) \quad (7)$$

The elemental morals are normalised admittances, and the impedances are decided by the system of Equations for a regard Resistive $Z_0 = 50$ ohm (8).

$$Z_A = Z_B = Z_0$$

$$Z_i = Z_0/g_i \quad (8)$$

$$Z_{j,1+1} = Z_0/J_{i,1+1}$$

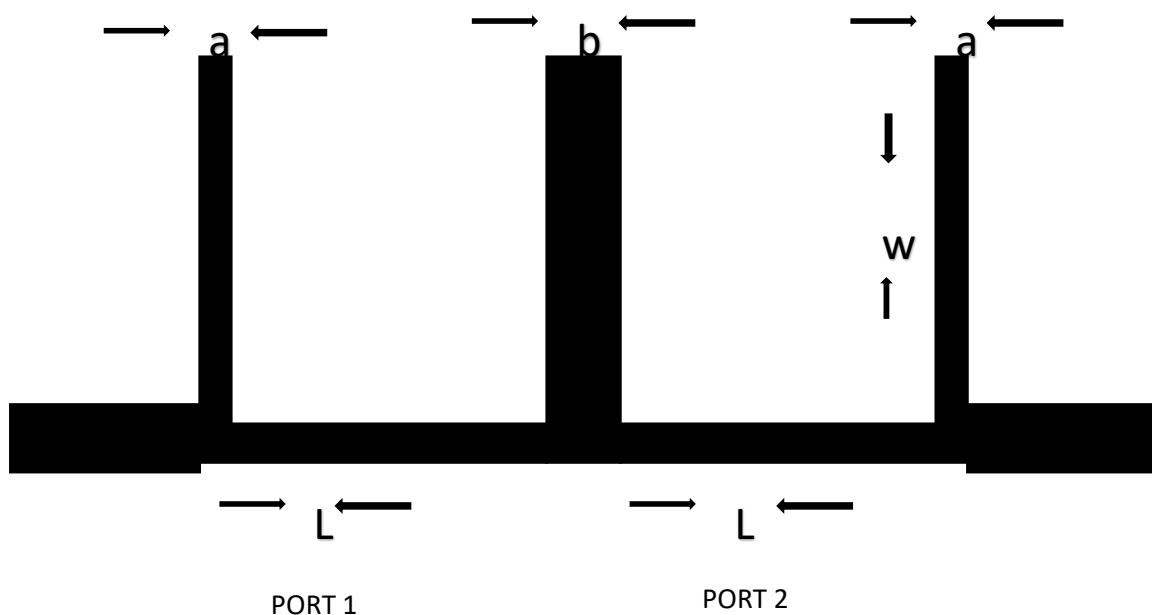


Fig 1 Design of the Low Pass Filter

The durations and widths of an associated micro-strip door open stub sift are calculated. The dimensions of such a micro strip line BSF design. The free end as well as T-junction effects are accounted for in the micro strip filtration depicted. The size of the micro-strip lines connected by two open end stubs is 0.45 mm, while the width of a 50-ohm micro-strip connection is 1.82 mm.

The fractal structure has now been implemented in the structure. The fractal curve is used to modify the thin micro-strip line. The proposed filter is shown. The dimensions of the modified filter remain unchanged; just the formation of connecting lines has been altered. The distance between two open end stubs is cut in half by using the Ketch fractal. $L = 15.5$ mm is indeed the ttf reduction achieved.

3. RESULT AND DISCUSSION

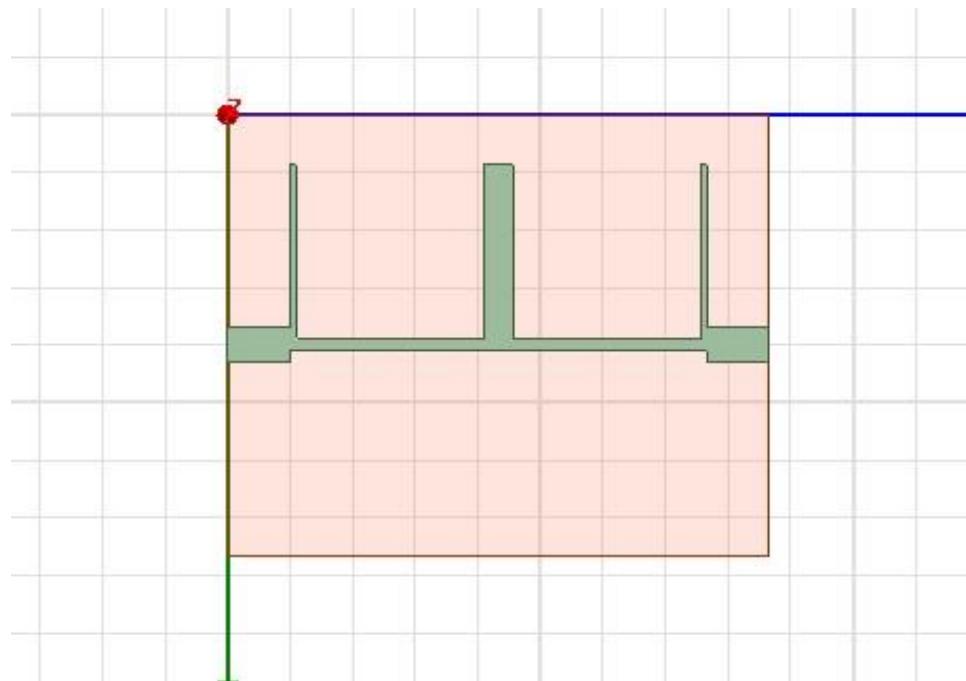


Fig 2 Ansys design

S11 PARAMETER

In practise, a most commonly quoted antenna parameter is S11. S11 represents the amount of power mirrored from the antenna and is thus known as the coefficient of reflection (also documented as radiation: or return loss). If $S11=0$ dB, the antenna reflects all of the power and emits nothing.

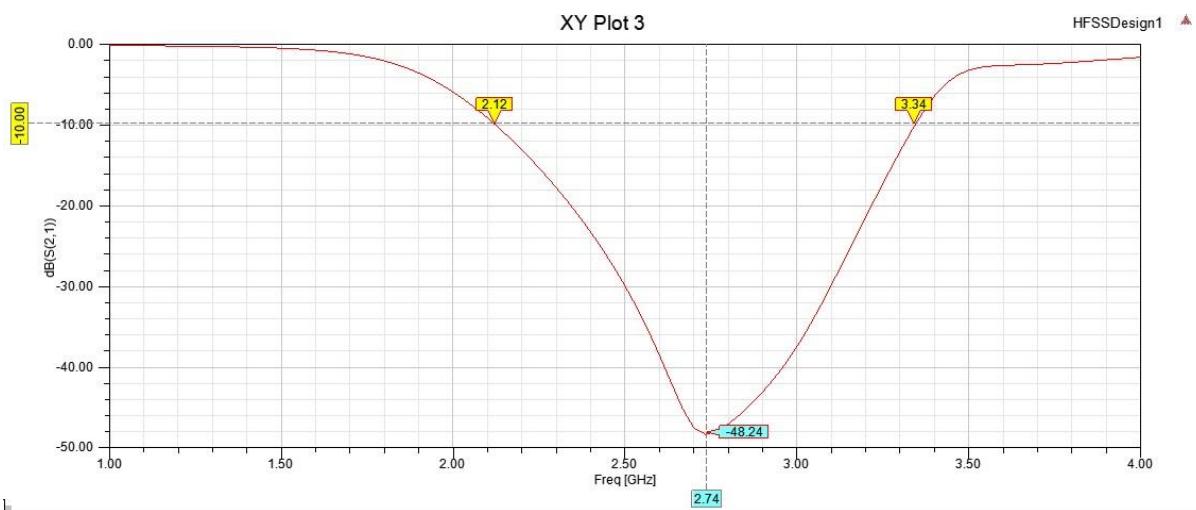


Fig 3 Reflection Coefficient

S21 PARAMETER

This is among S-parameters commonly used to characterise two-port networks. An S-parameter represents the amount of electricity having left one network port in relation to the amount of strength entering someone else (or the same) network port.

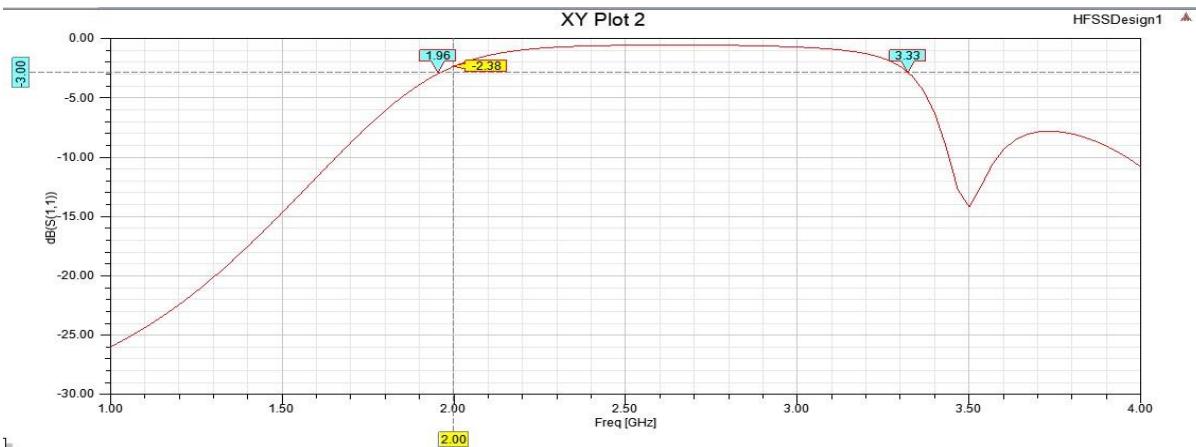


Fig 4 Transmission Coefficient

PARAMETERS ANALYSIS

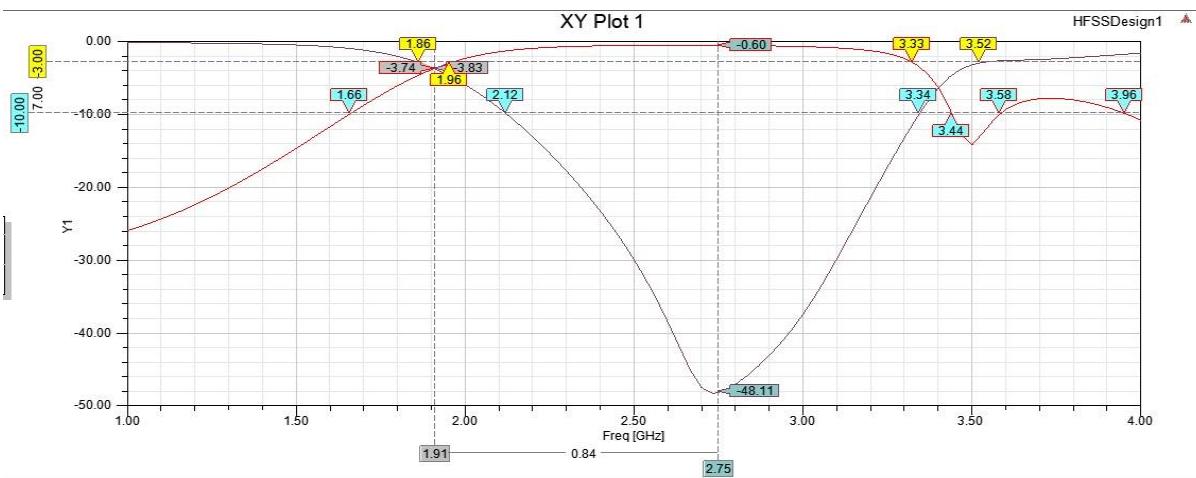


Fig 5 Simulation

The outputs of the design, simulation, and measurement are presented. The model is designed and built on a FR4 Epoxy mm - wave dielectric board ($\epsilon_r = 4.4$ and $\tan \delta = 0.02$), with the prototype's centre frequency 'f 0' set to 5 GHz. The measured and simulated output of the filters is shown above. To account for open ports and the dispersion effect of microstrip line lines, additional adjustments and optimization must be conducted in the HFSS after final software design. The physical size of the substrate for the configuration is 18mm x 15.5mm x 1.6mm, and the pass band of this filter is 0.22 GHz, with

a frequency of 5 GHz, which is used for wireless technology in the this WSN and RFID application. The rectangle slot is packed to FR4 epoxy substrate in the first case, and a different substrate is placed on top. For comparison, the reasoned S-parameter is plotted alongside the simulated result utilising Ansys HFSS. The calculated and observed results agree very well. The evaluated 3 dB corresponds to 5 GHz.

4. CONCLUSION

The method proposed is a simple, efficient, and efficient size reduction technique. This technique can benefit the majority of edge micro strip circuits. The size of the presented work was lowered by much more over 46.5 % without impacting the response when compared to the standard optimised band stop filtration system. In the response to a decrease pass filter, the proposed methodology achieves a small design while retaining the very same response as a conventional filter. In the response to a decrease pass filter, the size reduction is more than 26%. Following functions or optimization are not required for this method. The approach is validated by comparing simulated and measured results, which show strong agreement.

5. REFERENCE

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