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FINITE ELEMENT FOR SEISMIC ANALYSIS OF A PIPE LINE

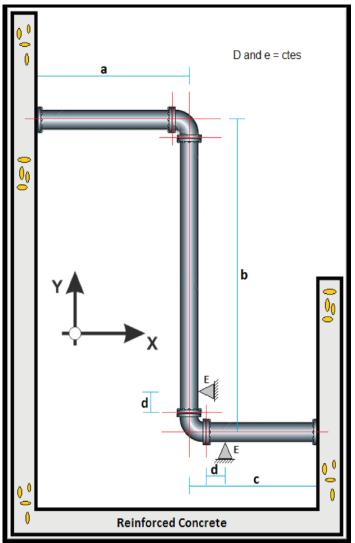
Amr Abbas¹

¹Mechanical Engineering, Mississippi State University, USA. DOI: https://www.doi.org/10.58257/IJPREMS32128

ABSTRACT

The target of this Study is to execute a a seismic analysis (response spectrum analysis) of a Pipe Line with the Performing of initially a static analysis of the pipe line considering its self-weight. Then Perform a modal analysis and obtain the natural frequencies and eigenvectors. Then Perform response spectrum analyses of the pipeline separately for the directions X, Y and Z. The solution is extended to perform Combine solution and Check Integrity & Sanity . The Analysis will be conducted with Patran Nastran.

.The System is presented as per Trailing



1. INTRODUCTION

Modal analysis is the process of identifying a system's natural frequencies, damping factors, and mode shapes in order to use them to create a mathematical model of the system's dynamic behavior. While Spectrum Analysis plot of the maximum response (maximum displacement, velocity, acceleration or any other quantity of interest) to a specified dynamic loading applied on all possible cases . The Dynamic behavior of piping systems is tremendously import specially when it is connected to high speed high value rotating equipment and the adjustment of the piping system dynamics is mandatory for smooth operation. In this study the Patran uses finite element analysis to calculate the dynamics of piping system from two prospectives Modal Analysis & Spectrum Analysis and the behaviors are compared as what is going to be detailed in this study



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2. SOLUTION METHODOLOGY

- 1. Perform a static analysis of the pipe line considering its self-weight.
- 2. Perform a modal analysis and obtain the natural frequencies and eigenvectors.
- 3. Perform response spectrum analyses of the pipe line separately for the directions X, Y and Z.
- 4. Combine step 1 and the three results of step 3 and obtain the combined result
- 5. Check if the pipe line maintains integrity
- 6. Sanity Checks

Data of interest

• The section has the following values for the defined parameters

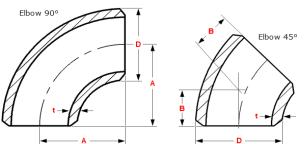
Parameter	Value	Unit	Meaning			
а	10	m				
b	20	m	Distances delimited in the figure			
c 8		m	Distances delimited in the figure			
d	1.5	m	1			
D	40	inch	Diameter of the pipe (*)			
е	STD	-	Pipe wall thickness (*)			

• Modal damping in the spectrum analysis of 5%.

Frequency (Hz)	Accelerations (g)			
0.10	0.0035			
0.25	0.0333			
0.40	0.0801			
1.00	0.3117			
1.42	0.4157			
2.00	0.5464			
2.82	0.6646			
3.98	0.7011			
5.62	0.7852			
7.94	0.7030			
11.22	0.5639			
15.84	0.4616			
22.39	0.3929			
31.62	0.3429			
34.00	0.3423			
100.00	0.3423			

Sanity checks

- Compare the reactions of the own weight analysis done with Patran with analytical calculation of model mass.
- Compare the frequencies obtained in the modal analysis with the ones obtained in the response spectrum analysis. Are there differences.
- Perform a static analysis applying the high acceleration of the spectrum as an inertial load. Compare the results with the ones obtained at the response spectrum analysis. Justify the comparative.
- 3. GEOMETRY CREATION



• We Will Take the Long Radius with thickness 10mm D= 1015 & A=1500 mm and generate The curve and chain it as one curve



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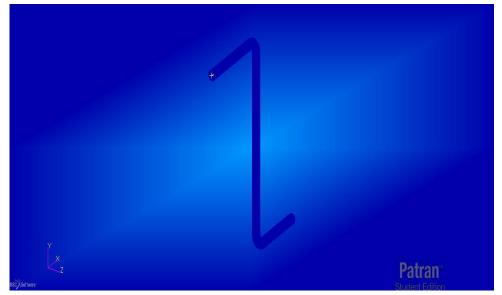
4. MATERIALS, PROPERTIES AND ELEMENTS

See the next table for materials, properties and element types used in the model.

	Part			Property	Element		
	1 41 t	Е	Poisson	Density	Damping Coeff.	Toperty	Element
	Pipe	2,00E+11	0,3	7850	0,05	1D Beam	Bar2

MESHING

As Indicated we will mesh the chained curve with the element Bar2, with around 4800 Elements & Nodes.

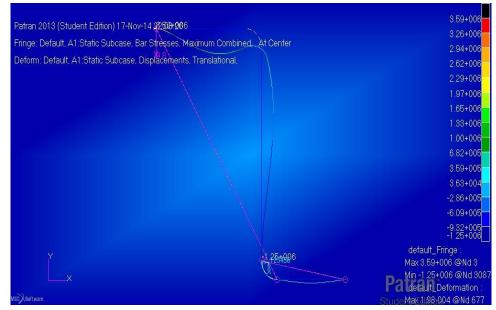


Loads And Boundary Conditions

Will create a RBE2 and set at the independent node an embedment. The Independent node will be a new node located at the intersection of lines connecting embedment and embedments as dependent nodes Then, let's create a fixed support at the independent node. Both inertial load and fixed support are stored at the "self-weight" load case.

5. SELF WEIGHT ANALYSIS

As it's said at the statement we have to solve the own-weight load case and then combine it with the spectral analysis. Therefore let's solve first the self-weight load case



Max Combined stress for self weight case

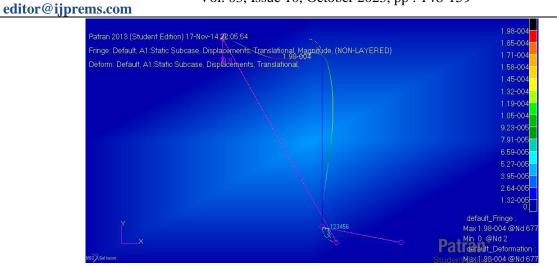


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Displacement of the Self Weight Case

6. SPECTRUM ANALYSIS. CONFIGURATION

We have analyzed the self-weight load case, and the scope of the model has been fixed. We will study the spectrum analysis having in mind these results.

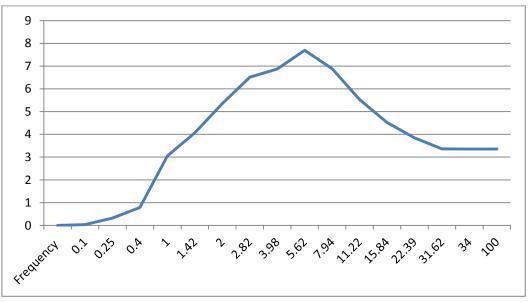
"TABLED1,2" This card defines the frequencies vs. acceleration spectrum.(It will change depending on Y , Z direction)

TABLED1, 2

 $+,\,0.1,\,0.0343,\,0.25,\,0.3263,\,0.4,\,0.7851,\,1,\,3.0547$

+, 2, 5.3547, 3.98, 6.8708, 7.94, 6.8894, 11.22, 5.5262

+, 22.39, 3.3604, 34, 3.3545, 100, 3.3545, ENDT



The Frequency in X direction

Frequency	Acceleration	M/Sec sqX & Z direction	Y direction
0.1	0.0035	0.0343	0.0137
0.25	0.0333	0.3263	0.1305
0.4	0.0801	0.785	0.314
1	0.3117	3.0547	1.2219
1.42	0.4157	4.0739	1.6296

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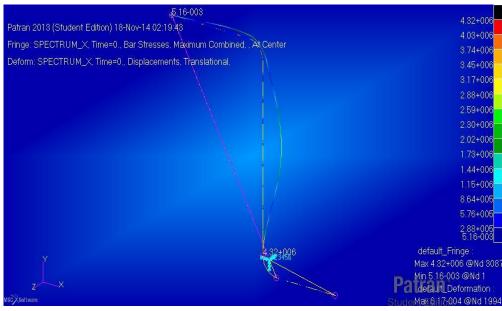
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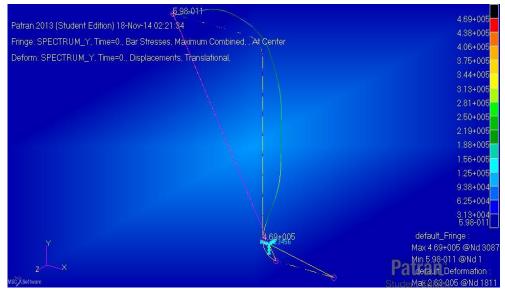
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	2	0.5464	5.3547	2.1419	
	2.82	0.6646	6.5131	2.6052	
	3.98	0.7011	6.8708	2.7483	
	5.62	0.7852	7.695	3.078	
	7.94	0.703	6.8894	2.7558	
	11.22	0.5639	5.5262	2.2105	
	15.84	0.4616	4.5237	1.8095	
	22.39	0.3929	3.8504	1.5402	
	31.62	0.3429	3.3604	1.3442	
	34	0.3423	3.3545	1.3418	
	100	0.3423	3.3545	1.3418	

7. SPECTRUM ANALYSIS. SOLUTION ANALYSIS

The following plots are the results in terms of stress tensor and displacements for Spectrum response in X, Y,Z AND COMBINED case.









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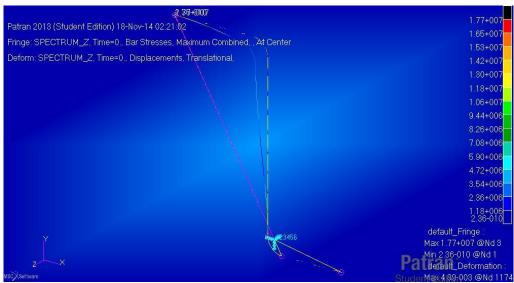
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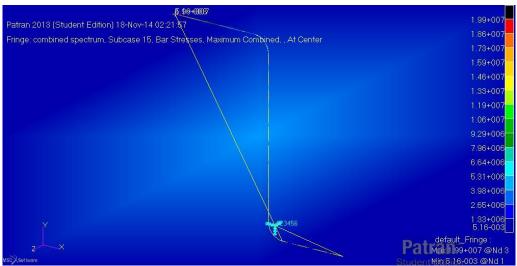
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Spectrum Y Direction

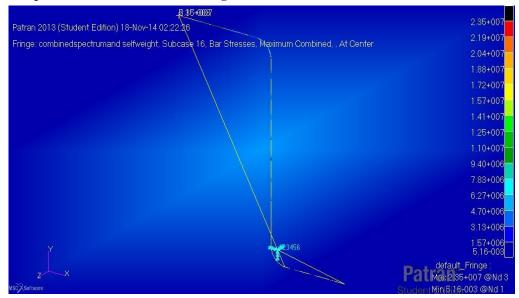


Spectrum Z Direction



Combined Spectrum

The combined spectrum combined with Self Weight





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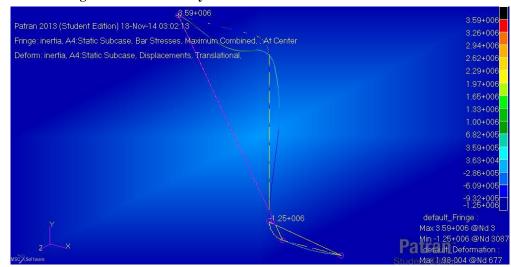
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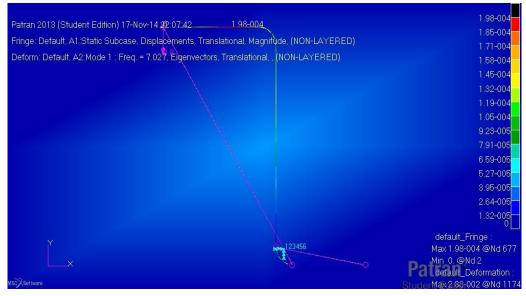
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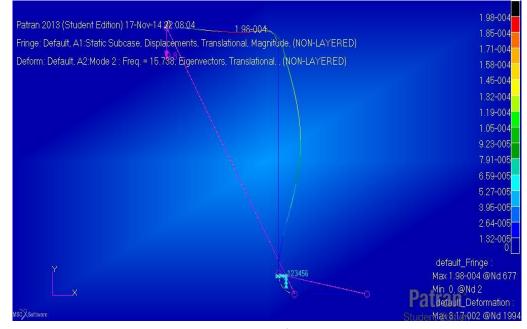
Inertia Case with the Highest value of Gravity acceleration



Modal Analysis Shape



Modal 1



Modal 2

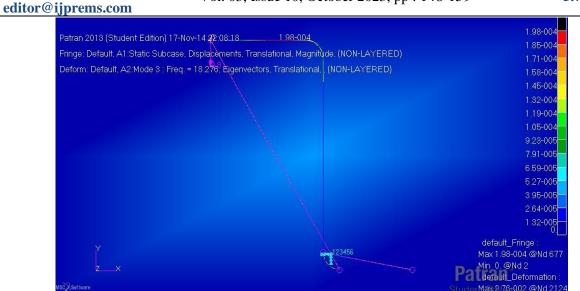


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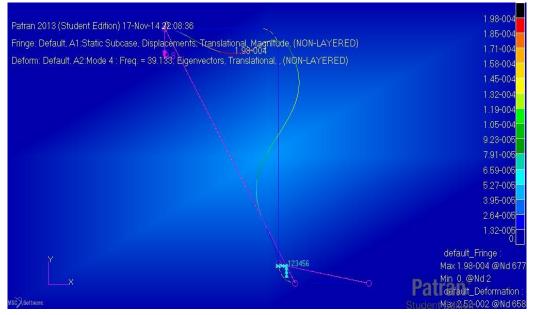
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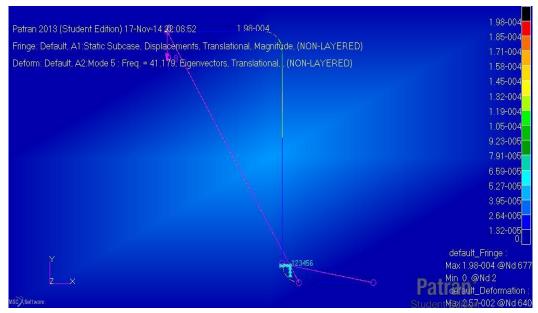
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Modal3



Modal 4



Modal 5

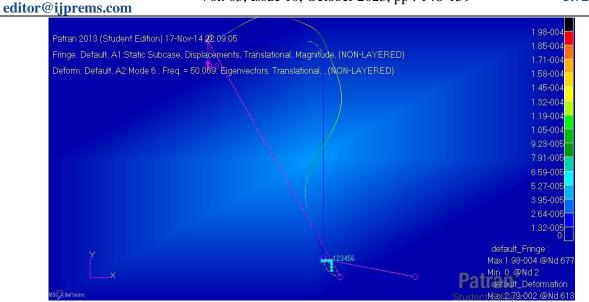


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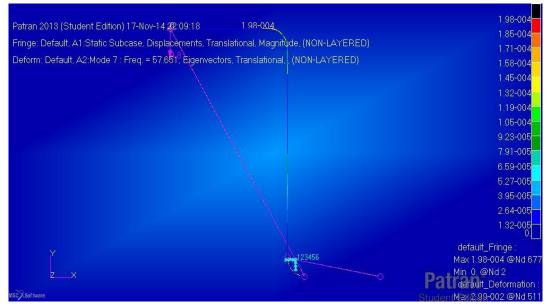
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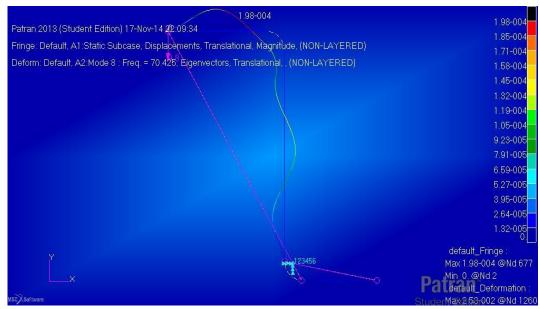
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Modal 6



Modal 7



Modal 8

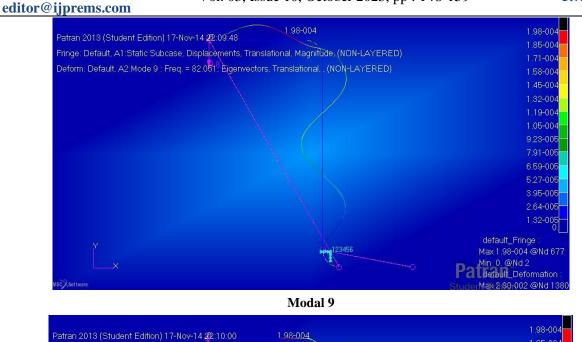


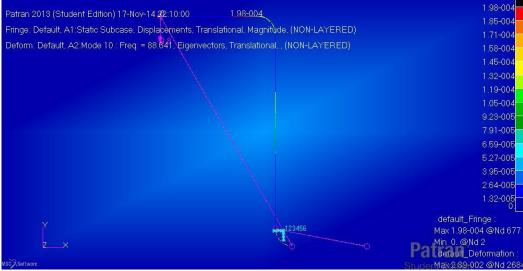
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Modal 10

8. SANITY CHECKS

1.1. VERTICAL REACTIONS. SELF-WEIGHT LOAD CASE

We can check the reactions given by Nastran at the embedment of the independent node of the RBE2. Extracting the Same from F06 File

weight							
radius out		0.507	Radius	. 0.80713386			
radius in		0.502	Radius	0.79129256			
		differ	ence in Area	0.015841			
	length		39)			
	volume		0.6178107	7			
	mass		4850)			
	weight		4.75E+04	Length 10+20+8+1 Mt for			
				Elbows			
FORCI	ES OI	FSIN	GLE-POINT	CONSTRAINT			
PO:	POINT ID. TYPE		T1	Т2 Т3			
	4081	G	-6.636314E-084.4	180734E+04 0.0			



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9. CHECKING FREQUENCIES

Below, we include the comparison between the normal modes obtained at a modal analysis and the normal modes obtained at the spectrum analysis,

	Spectrum Ret					rum Respon	ponse frequency			
MODE	DE EXTRACTION		EIGENVALUE RA		RADIANS			ERALIZED	GENERALIZED	
NO.). Order					MASS	STIFFNES	S		
1	1	0.0	0.0	0.0	1	.000000E+00	0.0			
2	2	1.94941	I3E+03	4.415216E4	01 7.0	27034E+00	1.000000E+	00 1.949	413E+03	
3	3	9.77817	9E+03	9.888467E4	01 1.5	73798E+01	1.000000E+	00 9.778	3179E+03	
4	4	1.31859	6E+04	1.148301E	02 1.8	27578E+01	1.000000E+	00 1.318	596E+04	
5	5	6.04574	18E+04	2.458810E4	02 3.9	13318E+01	1.000000E+	00 6.045	748E+04	
6	6	6.69429	8E+04	2.587334E4	62 4 .1	17870E+01	1.000000E+	00 6.694	298E+04	
7	7	9.89681	15E+04	3.145920E4	02 5.0	06888E+01	1.000000E+	00 9.896	815E+04	
8	8	1.31213	39E+05	3.622346E4	02 5.7	65143E+01	1.000000E+	00 1.312	139E+05	
9	9	1.95799	97E+05	4.424926E+	02 7.0	42487E+01	1.000000E+	00 1.957	997E+05	
10	10	2.6578	392E+05	5.155474E	+02 8.3	205192E+01	1.00 0 000E	+00 2.65	7892E+05	
11	11	3.1019	918E+05	5.569487E	+02 8.	864113E+01	1.00 0 000E	+ 0 0 3.10	1918E+05	
					Normal Modes					
MODE	EXTRA	CTION	EIGENVA	LUE	RADIANS	CYCLES	GEN	ERALIZED	GENERALIZED	
NO.	ORD	ER				MASS	STIFFNES	S		
1	1	1.94941	I3E+03	4.415216E	01 7.0	27034E+00	1.000000E+	00 1.949	413E+03	
2	2	9.77788	30E+03	9.888316E4	01 1.5	73774E+01	1.000000E+	00 9.777	880E+03	
3	3	1.31859	6E+04	1.148301E4	02 1.8	275 7 8E+01	1.000000E+	00 1.318	596E+04	
4	4	6.04574	48E+04	2.458810E4	02 3.9	13318E+01	1.000000E+	00 6.045	748E+04	
5	5	6 .6 9 429	98E+04	2.587334E4	62 4 .1	17870E+01	1.000000E+	00 6.694	298E+04	
6	6	9.89681	4E+04	3.145920E4	02 5.0	06887E+01	1.000000E+	00 9.896	814E+04	
7	7	1.31213	39E+05	3.622346E4	62 5.7	65143E+01	1.000000E+	00 1.312	139E+05	
8	8	1.95799	6E+05	4.424924E4	02 7.0	42486E+01	1.000000E+	00 1.957	996E+05	
9	9	2.65786	64E+05	5.155447E4	02 8.2	05149E+01	1.000000E+	00 2.657	864E+05	
10	10	3.1019	918E+05	5.569486E	+02 8.	864112E+01	1.00 0 000E	+ 0 0 3.10	1918E+05	

10. CONCLUSION

The study had compared the self-Weight case with Applied with this acceleration like an inertial load in a static load case, we obtain the results shown at above for value of Y direction the stresses is higher than the ones obtained at the spectral analysis (3.59e6 Pa the Static vs4.69e5 Pa the spectrum). This comparison verifies that the stress in the static inertial load case is higher than the spectrum case and the results of the spectral analysis are satisfactory. Also the Study had compared the Frequencies obtained from Spectrum Analysis & Modal Analysis with good match between values.

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